

# HEAVY LIFT & MARINE TRANSPORTATION ~EXPERIENCES SHARING

重件吊裝與海運經驗分享

February 2025

昱能海事股份有限公司 Wynnergy Marine Co., Ltd WYNNERGY MARINE 介紹

台灣離岸風電工作船與海事工程服務提供商:

●船舶投資 VESSEL INVESTMENT

●船舶租賃 VESSEL CHARTERING

●船舶設備供應
MARINE EQUIPMENT

●海事工程服務
MARINE ENGINEERING



























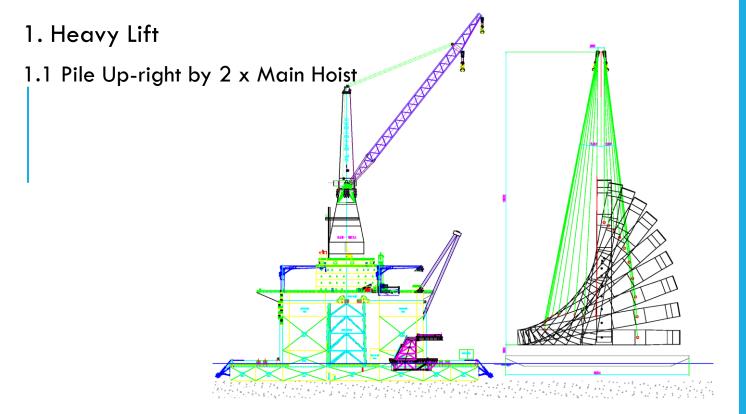
# WYNNERGY MARINE IN TAIWAN

### 2020~2024 Track Records in Taiwan

- PLGR, BOUY DEPLOYMENT and SEA HOTEL
- UWNM, ANCHOR HANDLING, HEAVY TRANSPORTATION, ECOLOGICAL OBSERVATIONS
- RESCUE STANDBY, CABLE LAYING GUARD, PILING OPERARTION GUARD, DRILLING GUARD, SCOUR PROTECTION GUARD

# 重件吊裝與海運經驗分享

- 1.Heavy Lift 重件吊裝
- 2.Marine Transportation 重件海運
- 3.Roll-on Loadout Operation 重件裝船



Up-right Angle	Wire Angle - Holding (dgr)	Wire Angle - Hoist Up (dgr)	Vertical Load - Holding (MT)	Vertical Load - Hoist Up (MT)	Hori. Load - Holding (MT)	Hori. Load - Hoist Up (MT)	Hook Load - Holding	Hook Load - Hoisting
0	79.081	83.312	372.371	612.629	71.835	71.835	379.237	616.826
10	78.783	82.920	379.335	605.665	75.226	75.226	386.722	610.319
20	78.861	82.736	387.088	597.912	76.216	76.216	394.520	602.750
30	79.330	82.821	394.648	590.352	74.357	74.357	401.592	595.016
40	80.189	83.240	400.594	584.406	69.274	69.274	406.539	588.498
50	81.422	84.044	402.736	582.264	60.750	60.750	407.292	585.425
60	82.995	85.252	397.298	587.702	48.818	48.818	400.286	589.726
70	84.861	86.821	376.078	608.922	33.824	33.824	377.596	609.861
80	86.980	88.599	312.035	672.965	16.460	16.460	312.469	673.166
90	90.000	90.000	0.000	985.000	0.000	0.000	0.000	985.000

- ZPMC Crane on 'ShunYi-1600'.
- Total Lifting Capacity 1600MT.
- Single Main Hoist Lifting Capacity 1200MT.
- Pile up-right by 2 x Main Hoist
- Pile Weight 985MT.

- Hook Load Calculations during up-righting to determine the following.
  - 1. Max. Hook Load within 2 Main Hoist.
- 2. Max. hook open up angle, must be less than allowable open up angle, normally 15°.

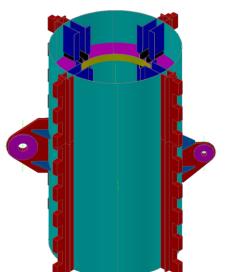
**Up-right Hook Load Calculation** 

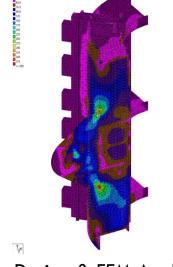
#### 1.2 Jack-up Barge Leg Removal

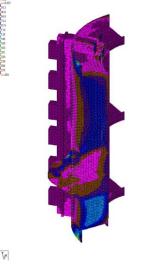












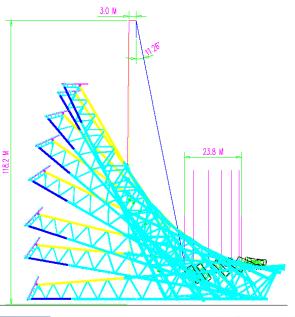
Padeye Design & FEM Analysis

- $1 \times Main Hoist + 1 \times Aux$ . Hoist to pull out.
- 2 x Main Hoist to Turn the leg level.
- Make it feasible to lift with limited hook height.
- Leg Weight 360MT each.

- $1 \times 400MT$  Padeye +  $2 \times 200MT$  Padeye.
- Padeye Strength Check by FEM Analysis.

#### 1.3 FPSO P54 Flare Boom Installation







#### P54 FLARE BOOM INSTALLATION BY SHEERLEG FLATING CRANE 'KAISEI'

Ming LI, Morline Pte Ltd, Singapore

#### SUMMARY

The Flare Boom weights 515 metric tons with a total height 93 meters from main deck at 65 degrees angle to horizontal, which is one of the largest and heaviest flare booms on FFSOs. It had been successfully installed in August 2007 by a 2050 MT floating sheerieg crane named 'Knisei', in Maua-Jurong Shipyard located at Rio de Janeiro, Brazil. There were 3 stages operation involved.

- Horizontally shift from Slip Way, rotate 90 degrees and laid onto wharf.
   Problems: Lifting off starting with Flare Boom at 3.2 degrees tilt to horizontal in Slip Way;
   Hydrotest water remained in the pipes causing running C.O.G.;
   Foul weather condition;
  - Foul weather condition; Landing on Supports with 4 degrees tilts.
- Install by 'Kaisei' using 2 main hooks.
   Problems: Mooring patterns for positioning 'Kaisei' 45 degrees to P54 vessel; Congested space on board 'P54' for manoeuvring during installation;

#### 1. INTRODUCTION

P54 is a FPSO vessel owned by Petrobras which was completed construction in October, 2007, in Maus-Jurong Shipyard at Rio de Janeiro, Brazil. The flare Boom is one of the largest, heaviest and highest the world so far among flare booms on FPSOs, semi-submersible rijes and fixed offshore platforms. The success of the Flare Boom installation on 2<sup>nd</sup> of Aug. 2007 was a milestone of completion of P54.

The final weight of the Flare Boom is 515 metric tons. It measures 108 meters in length when it was constructed on ground. It stands 91 meters tall from P54 main deck with 65 degrees slung to horizontal level.

The flare Boom was constructed inside the Slip Way in Maua-Jurong Shipyard. It was scated onto supports followed the tilt angle 3.2 degrees of the Slip Way. It was perpendicular to the Dock Gate with the bottom part to the sea. The 1" stage of the operation was to lift the Flare Boom out of the Slip Way, turn 90 degrees and place it parallel to the wharf at Quay 2, so that it could be uprighted at the 2" stage.

There are 2 padeyes located on top of the Flare Boom for up-righting and installation. The initial plan was to up-right by 2 main hooks from 'Kaisei'. But study showed it was not possible because the port side Main Hook Teet angle is more than allowable 15 degrees. A 250°T floating crane 'Plaui' was therefore called to assist for the operation.

The Flare Boom was installed successfully the following day at final stage. The mooring plan was well set up. The

Maua-Jurong Shipyard is located in Guanabara Bay. The swell from South West direction always affects a lot to the lifting operations. The installation date on 2<sup>ml</sup> of Aug., 2007 was selected in the good weather window period between the 2 storms.



Figure 1.1: P54 Location in Guanabara Bay

This paper will describe the problems and solutions during the lifting / installation process.

- Tandem Lift to lift and turn Flare Boom to 65°.
- 2 x Main Hoist to install Flare Boom to FPSO.
- Total Weight 515MT @93m High from main deck.

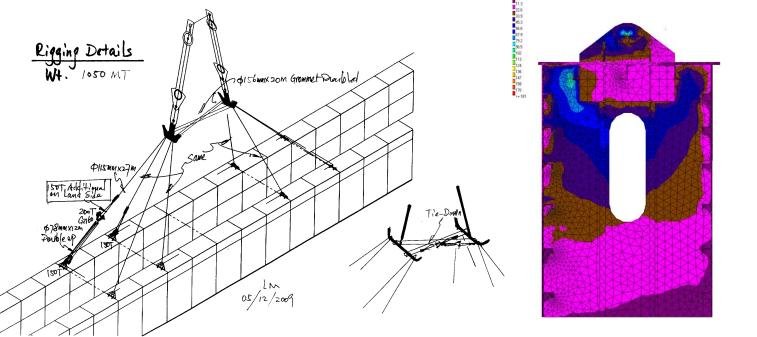
- The lifting operation was written in a report 'P54 Flare Boom Installation by Sheerleg Floating Crane 'Kaisei' and presented in RINA International Conference 'Marine Heavy Transport & Lift II – 2008'.

#### 1.4 Kone Crane Girder Installation





- Limited Hook Height.
- $2 \times Main Hoist to install.$
- Total Weight 1050MT.



- Lifting Points Design for short rigging height.

#### 1.5 FPSO P68 & P70 Module Lifting by 'L-3602' at EJA, Brazil





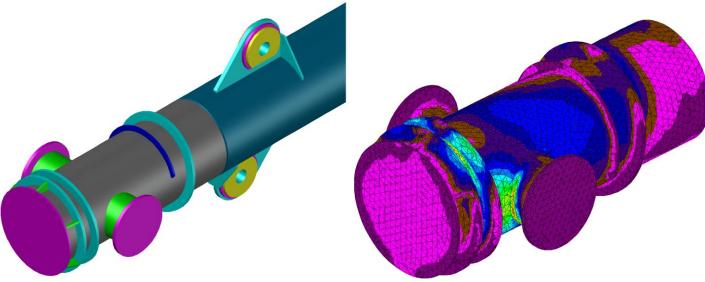
- 2 x spreader & 4 x Delta Plate by 4 x Main Hoist.
- Special designed rigging to make wire vertical to lifting points.
- Max. lifting Weight 2500MT for rigging design.

#### 1.6 FPSO 'Stybarrow' Mega Module Lifting









- Mega Module incl. of Port Module, Center Piperack & Stb'd Module.
- 8 x Padeyes.
- Inner Padeye takes double load of Outer Padeye.
- Special designed spreader SWL 1250MT x 33m.
- Max. Module Weight 2000MT.

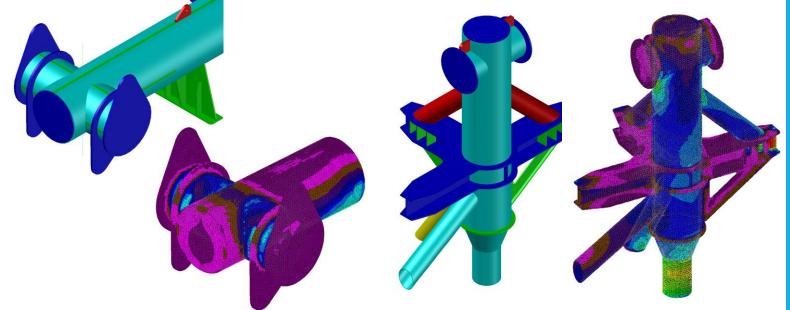
#### 1.7 FPSO 'Barossa' Module Lifting







- 4 to 6 lifting points.
- Trunnion as lifting point for modules over 3000MT.
- Spreader SWL 2500MT x 25m.
- Max. Module Weight 3850T.





**Up-right Lower Part** 







Inst. Top Part

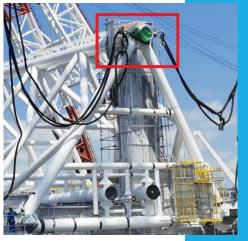
- 1.8 FPSO 'Barossa' Flare Tower Lifting

  - Up-right Middle Part Up-right Top Part

- Flare Tower in 3 parts, Lower, Middle & Upper.
- 4 lifting points at each part.
  - 1. Tailing
  - 2. 2 x Trunnion with Padeye
  - 3. Fixed
- Weight of each part.
  - 1. Lower Part 655MT
  - 2. Middle Part 217MT
  - 3. Upper Part 280MT
- Total Height from Vessel Deck 153m.







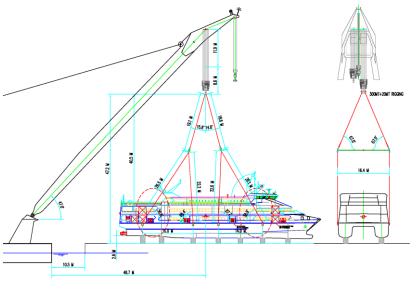
Tailing Point

Trunnion with Padeye

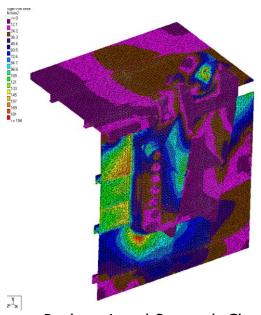
**Fixed Point** 

1.9 Catamaran Boat Lifting





Lifting Arrangement



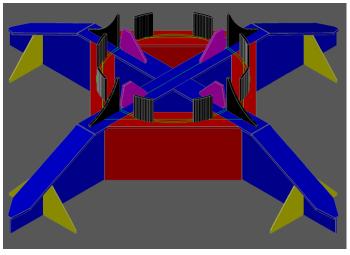
Padeye Local Strength Check

- Lift Catamaran from yard to water.
- Tow to Jurong Port
- Tandem Lift by 2 x Vessel Cranes
- Transport to Argentina

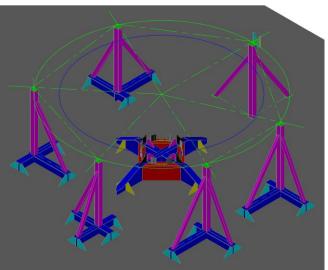
- Total Lifting Weight 300MT.

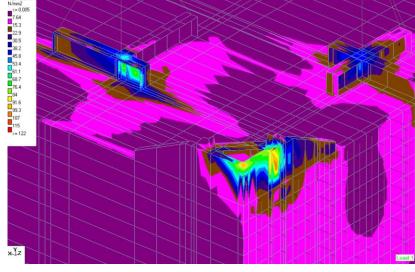
2.1 FPSO 'Pyrenees' Upper Turret Module (UTM)





Central Grillage Foundation





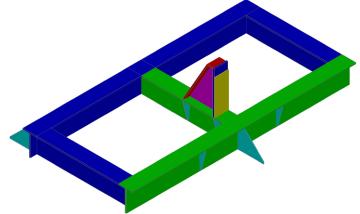
Overall View of Grillage

**Deck Strength Check** 

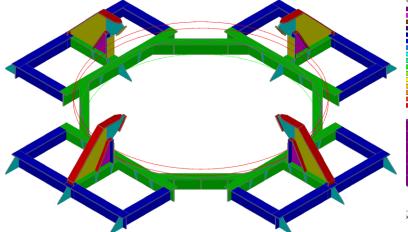
- Only UTM central column supports the whole weight of UTM.
- The central grillage foundation is designed for.
- 1. Support the whole load from UTM central column.
  - 2. Spread the load onto barge deck.
  - 3. Lifting guides for installation of UTM
  - 4. Lash down UTM to the top of foundation.
- The 6 x vertical supports are to stabilize UTM.
- No welding allowed between UTM Bottom and top of grillage.
- Total Weight of UTM 504MT.
- Deck Strength Check by FEM analysis.
- Plate & Beam Model.
- FEM model incl. of barge structural members and grillage structure.

2.2 FPSO 'Pyrenees' Lower Turret Module (LTM)

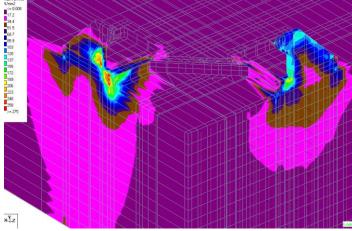




Installation Guide



Grillage & Lashing



**Deck Strength Check** 

- The grillage beams are in line with barge deck structural members.
- The grillage beams and installation guides are laid onto barge first to receive LTM by lifting.
- The lashing part will add on to the installation guide.
- Total Weight of LTM 503.5MT.

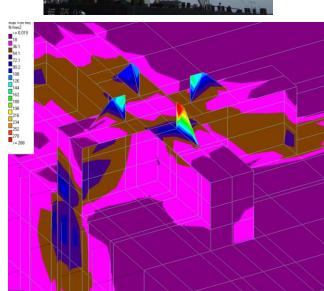
- Deck Strength Check by FEM analysis.
- Plate & Beam Model.
- FEM model incl. of barge structural members and grillage & lashing structure.

#### 2.3 FPSO 'Pyrenees' Swivel Access Support (SAS)









Grillage & Lashing

- The grillage beams are in line with barge deck structural members.
- Total Weight of SAS 312.9MT.

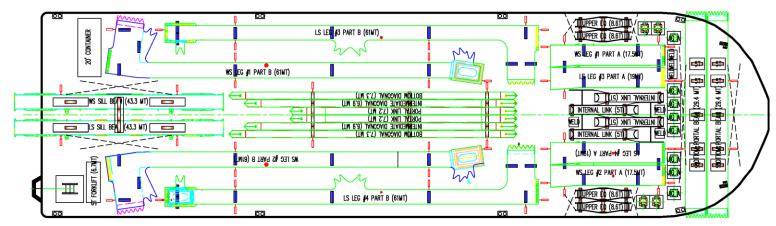
- Deck Strength Check by FEM analysis.
- Plate & Beam Model.
- FEM model incl. of barge structural members and grillage & lashing structure.

#### 2.4 Impsa Container Quay Crane Lower Frame Transported in Loose





After fully erected at PTP

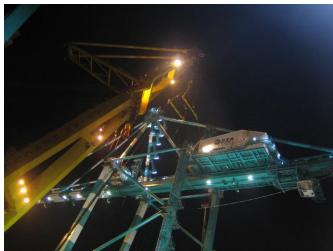


Stowage Plan of CQC Lower Frame Parts

- One CQC Lower Frame Parts are well organized on one barge.
- One set of grillages and lashings for  $3 \times CQC$  Lower Parts in 3 shipments.

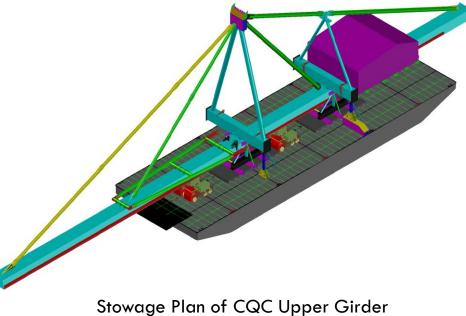
2.5 Impsa Container Quay Crane Upper Girger



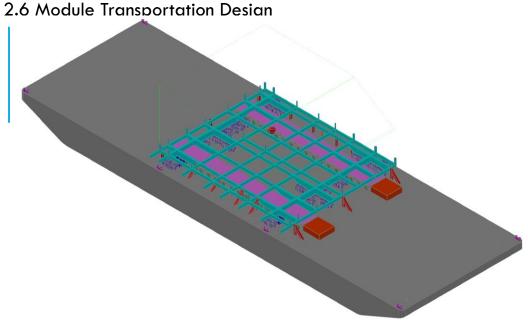


Installed by Floating Crane

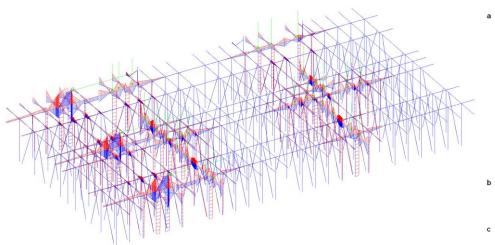




- CQC Upper Girder was roll-on to barge.
- It was measured 140m long, weighing 1200MT.
- Only pipe lashing.
- Stool supports on loadout beams.
- CQC Girder was installed by 'Asian Hercules II'



Stowage Plan – E House Module



**Deck Strength Check** 

- The Marine Transportation design normally incl. of the following drawings and calculations.
  - 1. Stowage Plan
  - 2. Lashing Design & Lashing Strength Check
  - 3. Vessel Deck Strength FEM Analysis
  - 4. Intact & Damage Stability Calculation\*
  - 5. Towing Capacity Check\*
- \*4. One tank damage.
- \*5. In 2 weather conditions, severe condition for holding vessel in position, and normal condition for towing speed estimation.

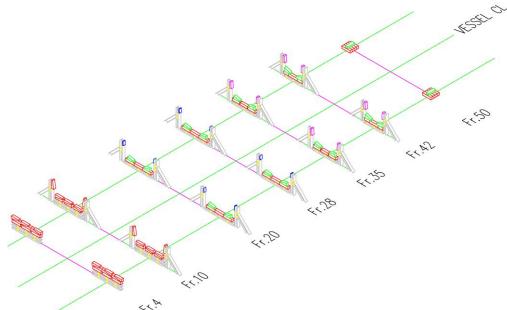
#### E-house Transportation Lashing Calculation Guideline for Marine Transportations, Report No.0014/NDI, Noble Denton

1	Load Resulting from Vessel Motions							
•	Load Resulting Iron vesser Motions							
a	General Information							
	Cargo Barge Length OA	76.200	meters					
	Cargo Barge Beam	24.320	meters					
	Cargo Barge Depth	4.877	meters					
	Rolling Angle Applied	10.0	degrees in	degrees in 10 seconds full cycle period				
	Pitching Angle Applied	10.0	degrees in	10 seconds	full cycle period			
	Heave Acceleration (g)	0.1	m/s^2					
	Draft of Cargo Barge	1.51	meters					
	Cargo Weight	849.11	MT					
	Trans. Dist to Barge CL (Y)	0.000	meters					
	Longi. Dist to barge CL (X)	0.000	meters					
	Cargo VCG to Deck (Z)	6.100	meters					
	Cargo Length in longitudinal Direction	26.250	meters					
	Cargo Width in Transververse Direction	23.000	meters					
	Cargo Height to Deck	13.000	meters					
	Uplift Lever in X	10.050	meters					
	Uplift Lever in Y	9.652	meters					
b	Condition A :	Roll & Heave						
			Roll+Heave co	eleration (a)	Roll-Heave \co	eleration (a)		
	Vertical Load (KN)		9023.543	1.08	7382.899	1.08		
	Transverse Load (KN)	:	2143.673	0.26	1854.383	0.26		
c	Condition B :	Pitch & Heave						
•	condition b .		itch+Heaveceleration (g)		Pitch-Heave Acceleration (g)			
	Vertical Load		9023 543	1.08	7382 899	1.08		
	Longitudinal Load	-	2143.673	0.26	1854.383	0.26		
-	Longitudinal Load		2143.073		1004.000	0.20		

#### 2.7 Catamaran Grillage & Lashing Design

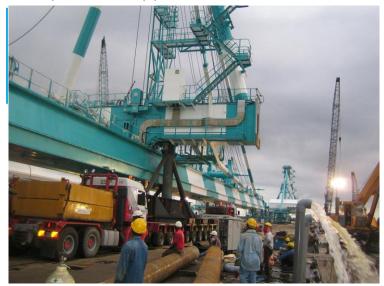


Grillage & Lashing on Deck



- Wooden grillage in line with vessel deck and catamaran strong structural members.
- Wooden grillage is adjustable to suit the shape of catamaran bottom.
- I Beam stanchions as lashing in vessel trans. direction.
- Crossed wire lashings added after Catamaran fully seated.

- 3. Roll-on Loadout Operation
- 3.1 Impsa CQC Upper Girder Loadout





Ballasting Tanks during Roll-on Operation

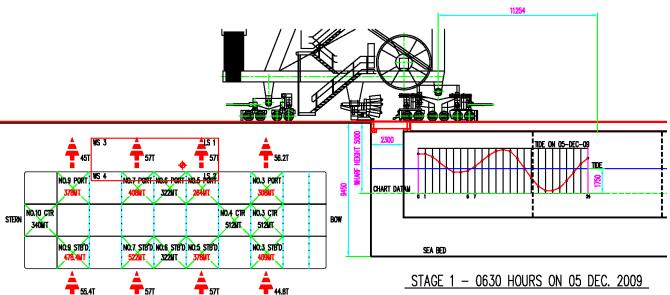
- In general the Roll-on operation design should consider the following.
  - 1. Roll-on operation normally at rising tide.
  - 2. Mooring is crucial to secure the barge.
- 3. Water Depth, wharf height and local tide table be taken into account for roll-on stability calculation.
- 4. Ramp / Bridge is required for connecting shore to barge.
- 5. Barge ballasting tanks are for level up barge during roll-on and encounter the tideal difference.
- 6. Ballast pump capacities be sufficient for roll-on in planned period, and encounter tidal range within 24 hours daily if roll-on got stuck in halfway.
- 7. No. of pumps should be 50% more than working pumps for standby.
- 8. Electrical pumps need 2 independent power supplies.

#### 3. Roll-on Loadout Operation

#### 3.2 Coat Unloader Loadout



## Ballast Calculation



- Barge port side alongside for side loading.
- Port tanks de-ballast out while stb'd tanks ballast in.

Ballast on Tanks when front Bogies Cross Over

## **CONCLUSION REMARKS**





Design ability is crucial and we hope to introduce the design package to assist the local development of Taiwan offshore wind industry.



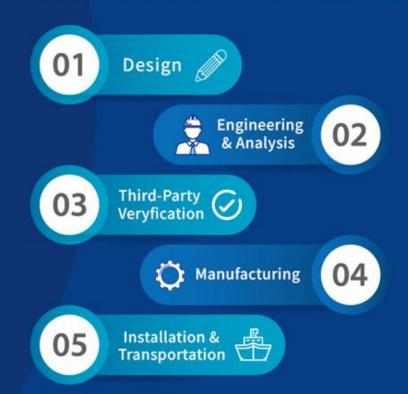
Not only the design tools but also the experienced engineering team to deal with the lifting(padeyes and spreaders design), roll on, loadout, sea fastening and marine transportation cases.



Meet the requirements from regulatory bodies and 3<sup>rd</sup> party and also provide the cost-effective design package.

# Thank you for listening

Heavy lifting & Marine transportation Solution for Taiwan offshore wind industry



We have experienced industry experts and an engineering team with extensive experience and a thorough understanding of the standards set by regulatory regulatory authorities for Heavy lifting and Marine transportation, ensuring we meet the requirements of our clients and their principals.

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- Marine Equipment
- Marine Engineering

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